

**Logging of Performance of my Geothermal Heat Pump
GeoMax2 from Heat Controller Inc**
(Permanently on low power mode)

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INTRODUCTION

When building my home in NY I had no luck in finding any heating installer (with knowledge) who believed that geothermal heat pumps work in Clinton County. I know locally they have a bad reputation because of past failures due to improper installation. In the end I had to learn a lot more about heat pumps than I ever thought I needed to know so that I could install it myself with the aid of an installer willing to learn about heat pumps. Installers said things like: 'they don't work here', 'they use too much electricity and cost too much to run', 'open loop systems aren't advised', 'in forced air applications they don't heat the air enough to work', 'you will pump your well dry...they use a million gallons of water a year', 'manufactures exaggerate performance so they won't work as well as they say' etc.

Well, as a scientist-engineer I was not convinced so I decided to install one against local advice AND use my laboratory equipment to check performance as a reality check and 'science project'.

EXECUTIVE SUMMARY: My open loop heat pump went on line in Jan 2008 and has been working just fine. In my 2000 sq ft home with standard insulation the HP will use 7,450 kWh of electricity in an 8010 HDD heating year at a cost of \$1,275, which is competitive with fuel oil costs at current market prices.

READ ON IF YOU WANT TO SEE THE PROOF

Basics of how a GHP works.

My HP draws in room air at T_{AirIn} and warms it up to a higher temperature, T_{AirOut} . The amount of heat supplied (HS) in BTU/h distributed to the house depends on the volume of air moved in (CFM = cubic feet per minute) and the amount of heat energy in the warmed air. The equation that applies to any hot air furnace (including a GHP) is:

$$HS = 1.06 \times CFM \times (T_{AirOut} - T_{AirIn}). \quad \text{Eq. 1}$$

A GHP extracts some of the heat sent to the house (in HS) from well water. A BTU is defined as the amount of energy needed to change one lb of water 1 °F. One gal of water weighs 8.35 lbs and if I pump at 1 GPM (gal per minute) I pump 500 lb/h (= 60 x 8.35). Hence the rate of heat extraction (HE) is given by

$$HE = 500 \times GPM \times \text{water temperature rise} \quad \text{OR} \\ HE = 500 \times GPM \times (T_{WaterIn} - T_{WaterOut}) \quad \text{(Eq. 2)}$$

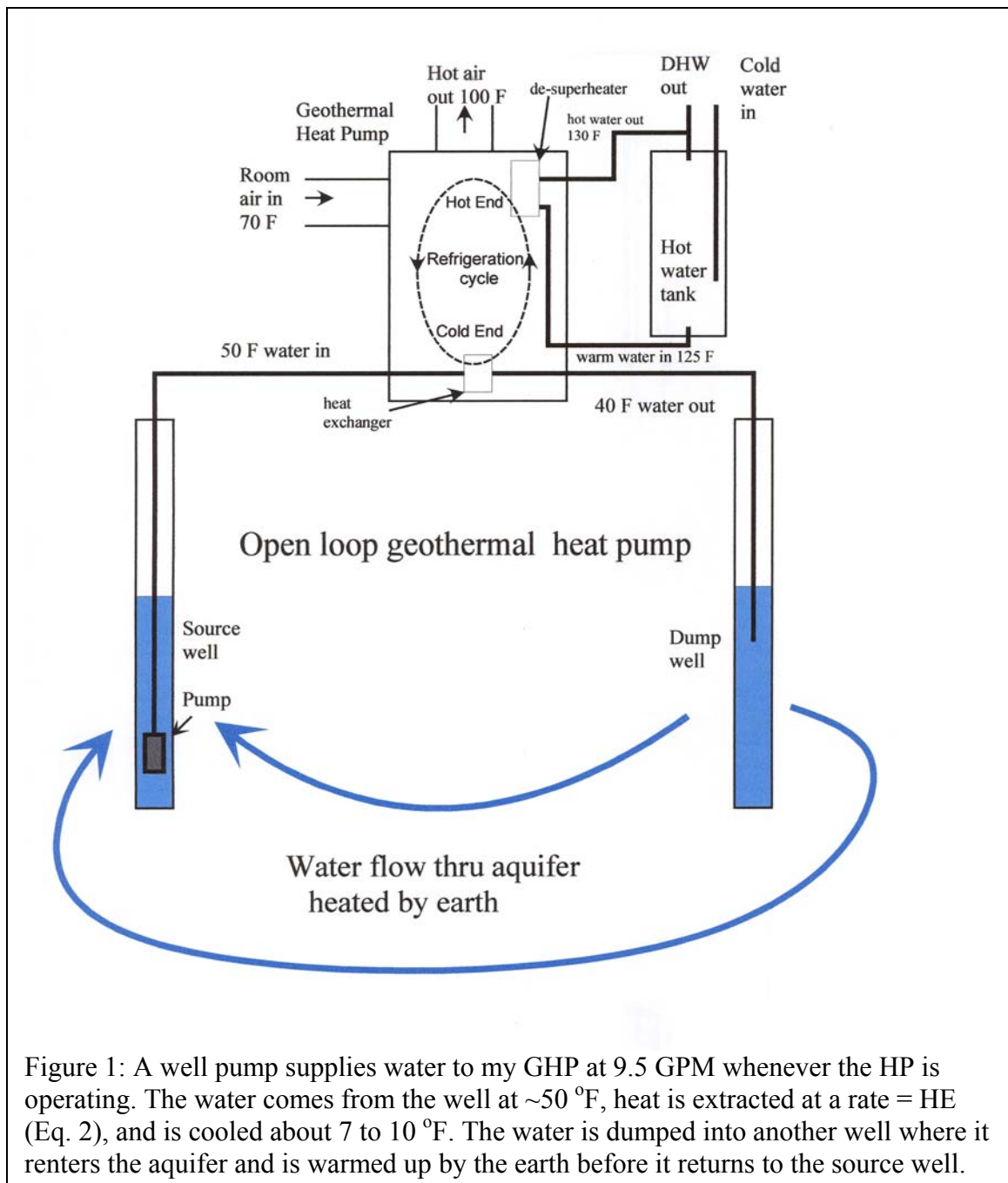
The temperature of the water falls during the heating season because the GHP is extracting water from the ground.

The whole process is illustrated in Fig. 1

The 'pumping' part of the GHP is provided by a refrigeration compressor that pumps freon gas/liquid (or its modern equivalent) through a refrigeration cycle. At the cold end, the freon is at low temperature (about 30 to 35 °F) and pressure and is colder than the well water hence it can extract heat via a heat exchanger. At the warm end, the freon is under high pressure and is warmer than the room air (125 to 135 °F) and hence can deliver warm air to the house through a heat exchanger; another heat exchanger also heats my hot water tank, providing assistance to my hot water tank. Electricity is used to drive the compressor adding some energy to the process (= EA = energy added), and some of this electrical energy goes to heat the air and to heat my hot water tank. Below are performance data I have measured. I installed temperature sensor to measure T_{AirIn} , T_{AirOut} , $T_{WaterIn}$, $T_{WaterOut}$. I installed a water flow meter to measure GPM. The GHP measures and reports CFM to within 5% accuracy. I also have a power meters to measure EA and the energy to drive my well pump. The overall accuracy of the measurements is probably about 10% because T measurements are accurate to only ± 0.5 °F.

COP = coefficient of performance = HS/EA.

Overall efficiency = $100\% \times HS/(EA + \text{the energy needed to run my well pump})$.



Methods

Measurements were done in my newly constructed home in Ellenburg, Clinton County, NY 12935. This home is heated with an open loop geothermal heat pump.

A Personal DAQ3005 was used to monitor DC voltages from various sensors (See <http://www.iotech.com/catalog/daq/persdaq3000.html>). Over the voltage ranges in this study the 16-bit DAQ3005 can measure to better than 0.01% of full scale. The GeoMax2 requires 230 VAC @ 20 A or less for normal operation. Power consumption (kW) of the

GeoMax2 was computed from RMS current (A) and voltage (V). To insure a more predictable performance the stage-2 heating was disabled by disconnecting the stage-2 control line between the thermostat and the GeoMax2 control panel. RMS current was measured with a model ACT, see:

http://web1.automationdirect.com/adc/Overview/Catalog/Sensors_-z-Encoders/Current_Sensing_Transducers/AC_Current_Transducers

The ACT coil was placed next to the circuit breaker on the service panel that supplies power to the GeoMax2. The coils were set to a calibration of 0-20 A = 0-10 VDC. RMS V was measured using a custom built circuit consisting of a 115 VAC to 12 VAC step down isolated transformer (0.35 watt) going to a full wave rectifier and terminated by a 25 K resistor going to a 40 μ F capacitor to ground in parallel with another 25 K resistor to ground. The DC output was calibrated with a Variac voltage transformer and a Digital VOM accurate to 0.2%. See Fig. 2 below.

Two of the above circuits were used to measure V_{AC1} and V_{AC2} , one to measure the RMS Voltage on each side of my service panel. Power was computed from:

$$\text{power} = A_{RMS} (V_{AC1} + V_{AC2})$$

Another ACT coil was used to measure current to my water pump. Since water has to be supplied to the GeoMax2 during operation, the power consumption of the water pump is an important part of the energy requirement of geothermal heating.

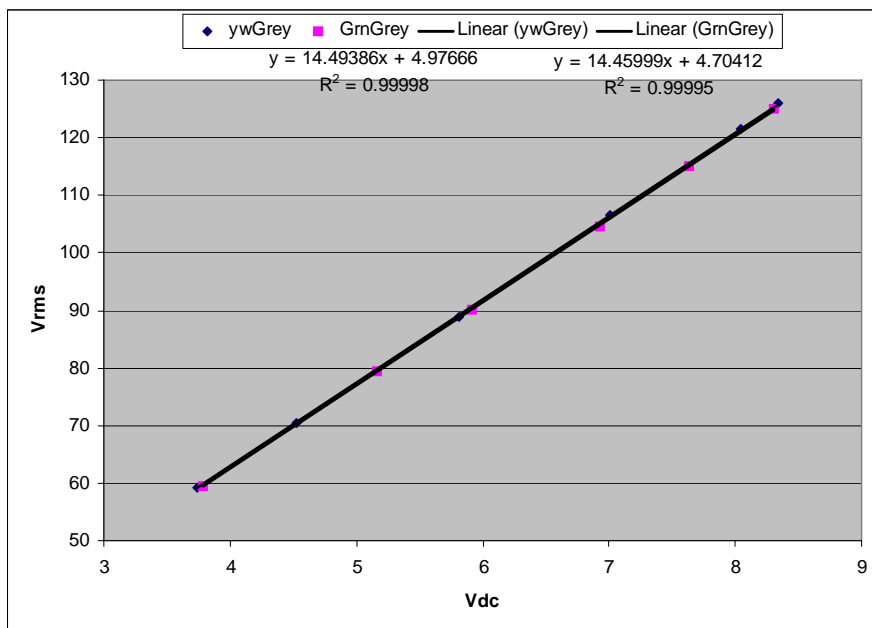


Fig. 2: Typical calibration of my custom-built sensor for converting V_{RMS} to V DC. The normal operating range is 110 to 120 V AC @ 60 Hz

Temperatures were also measured of (1) water flowing into the GeoMax2, (2) water flowing out of the GeoMax2, (3) air intake from the house into the GeoMax2 heat exchanger, (4) air discharge from the GeoMax2 to the house. Temperatures were measured using LM335 sensors calibrated to an output of 10 mV/ $^{\circ}$ K, hence 0 $^{\circ}$ C

corresponded to a voltage of 2.7316 V DC and 20 °C to 2.9316 V DC. A high sampling rate per second averaged every second insured temperature measurements to ± 0.1 °C (± 0.2 °F)

All DC sensor voltages were logged on the DAQ3005 at the rate of 200 measurements per second and averages of 200 readings were saved on a computer once per second, thus permitting a second-by-second evaluation of power (kW) and energy (kWh) usage.

Water supply to the GeoMax2 was provided at 9.5 GPM, however pump pressure variations resulted in a variation of flow from about 9.2 to 9.8 GPM. Water flow was monitored manually with a basic inline water flow meter accurate to 2.5% in mid-range (<http://www.lakemonitors.com/basicinline.htm>). The Geomax2 regulated air flow thorough a variable power ECM Motor and normally supplies air at 1500 CFM $\pm 5\%$. (GPM = gallons per minute, CFM = cubic feet per minute).

Local climate was measured with a Davis Vantage Pro2 Plus wireless weather station: http://www.davisnet.com/weather/products/vantage2_plus.asp This station measured air temperature in a fan-aspirated weather shield mounted on a tower 300 ft from the house. Data were logged with Virtual Weather Station software every 5 s, which produced daily reports including heating degree days HDD base 65 °F.

Results & Discussion

Power up sequence

From 30 April to 13 May 2008 the GeoMax2 powered up 451 times. The power use versus time is shown below:

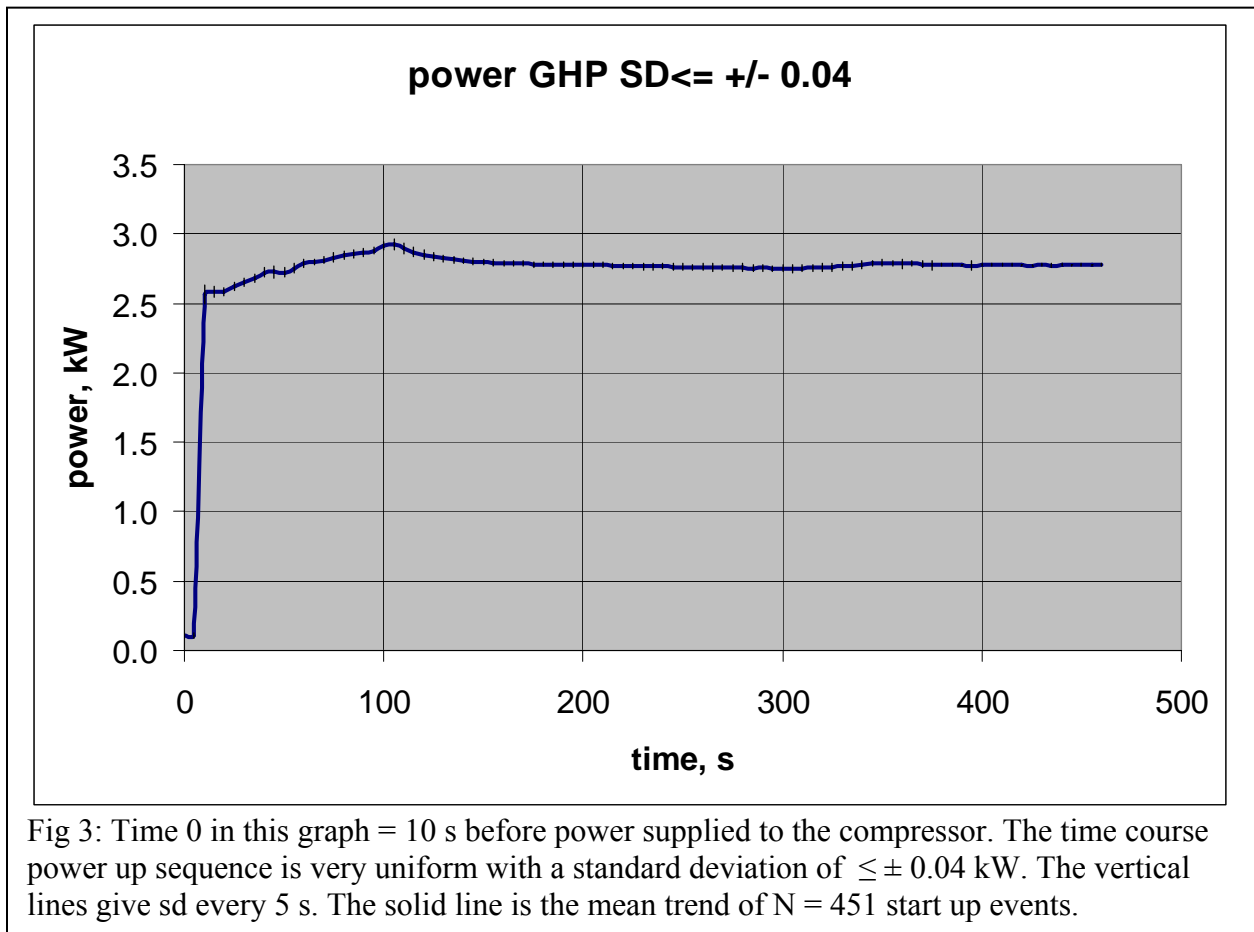
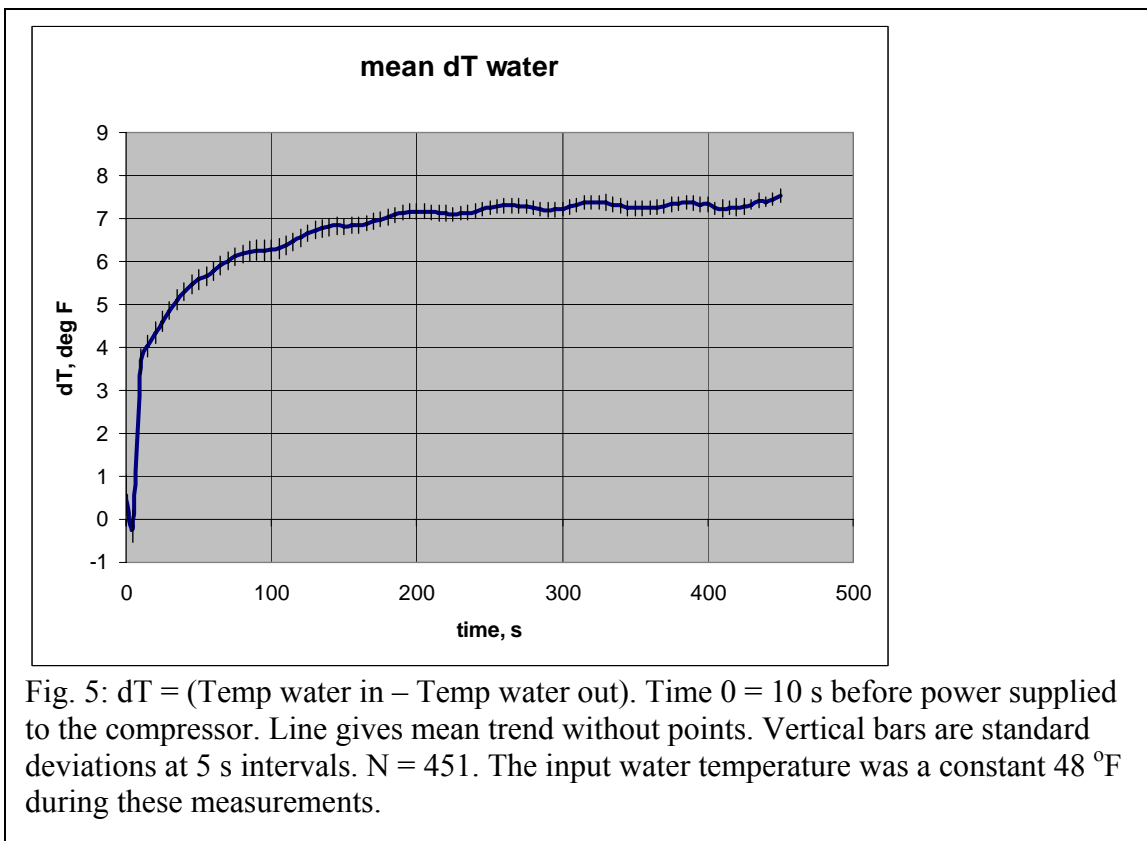
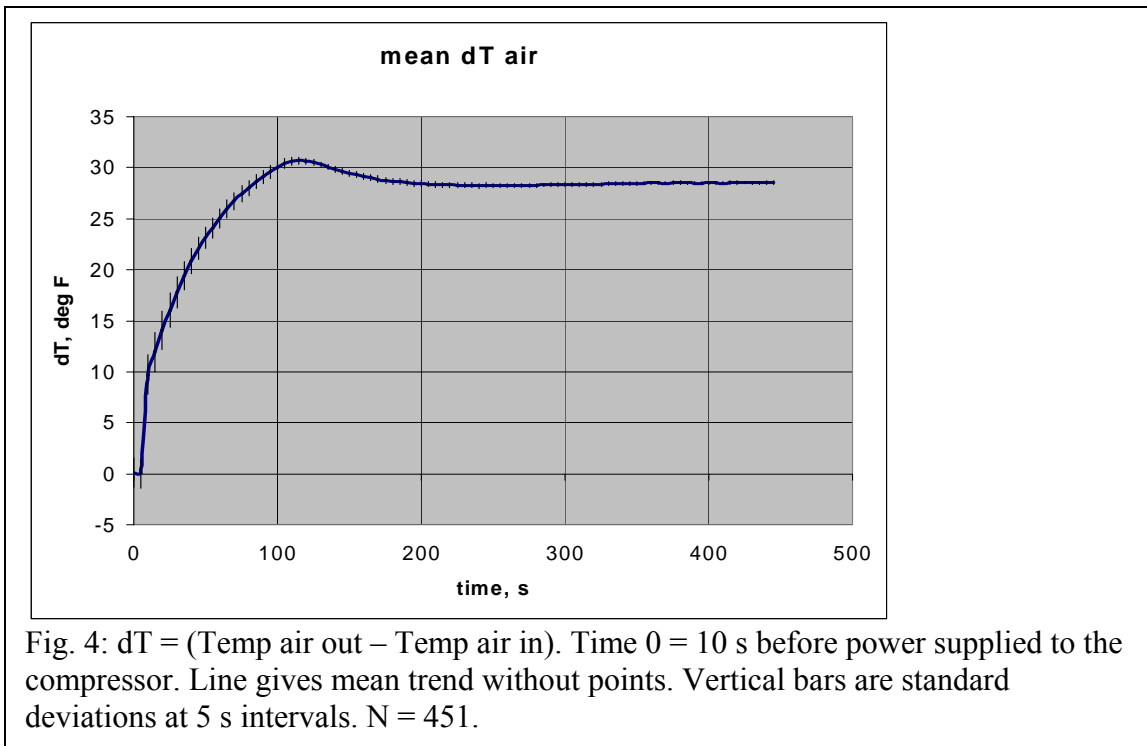


Fig 3: Time 0 in this graph = 10 s before power supplied to the compressor. The time course power up sequence is very uniform with a standard deviation of $\leq \pm 0.04$ kW. The vertical lines give sd every 5 s. The solid line is the mean trend of $N = 451$ start up events.

The corresponding changes in air temperature and water changes are given in Figs 4 and 5 respectively.



Power up sequence: Discussion

The GeoMax2 extracts heat from well water thus lowering the temperature of the water. The heat-energy unit most frequently used in the USA is the BTU (British Thermal Unit), which is defined as the amount of heat needed to change 1 pound of water by 1 °F. Since one gallon of water weights 8.35 lb, BTU/h can be computed from

$$\text{BTU/h} = 500 \text{ GPM} * dT_{\text{water}},$$

because $8.35 \text{ lb} \times 60 \text{ min/h} = 500$. Since the mean dT_{water} after 300 s is about 7.3 °F the rate of heat extraction (HE) from the well water is

$$\text{HE} = 500 \times 9.5 \times 7.3 = 34,575 \text{ BTU/h.}$$

The accuracy of this measurement is limited by the accuracy of water-flow measurement ($\pm 2.5\%$) and water temperature measurement (± 0.2 °F out of $7.3 \cong \pm 3\%$). The combined error (E) of two numbers multiplied or divided is given by $E\% = \sqrt{A^2 + B^2}$, where A and B are the individual errors. So the combined error is about 4%, hence the value plus error of $\text{HE} = 34,575 \pm 1350$.

The corresponding formula for heat discharge to the house is

$$\text{BTU/h} = 1.06 \text{ CFM} dT_{\text{air}},$$

Since the mean GeoMax2 pumps air at 1500 CFM and $dT_{\text{air}} = 28.4$ °F after 300 s, the mean rate of heat supply (HS) to the house is given by

$$\text{HS} = 1.06 \times 1500 \text{ CFM} \times 28.4 = 45,160 \text{ BTU/h.}$$

The power consumption at 300 s = 2.75 kW and $1 \text{ kW} = 3,410 \text{ BTU/h}$, hence the GeoMax2 uses $2.75 \times 3410 = 9,378 \text{ BTU/h}$ of electrical energy to provide 45,160 BTU of heat to the house. This corresponds to a coefficient of performance of

$$\text{COP} = 45,160/9,378 = 4.82.$$

The combined uncertainty of absolute temperature measurement was about ± 0.2 °F out of 28 °F $\cong 0.7\%$, but the error in CFM $\cong 5\%$, hence the overall certainty on the COP is about 5.05%: $\text{COP} = 4.82 \pm 0.24$.

Energy consumption of the water pump vs the GeoMax2

The overall efficiency (E) of the GeoMax2 can be defined as:

$$E = 100\% \text{ HS}/(\text{P}_{\text{GM}} + \text{P}_{\text{WP}}),$$

Where P_{GM} = the power consumption of the GeoMax2 compressor and P_{WP} = the average power consumption of the water pump. However, the water pump turns on and off frequently (about once per minute) when the GeoMax2 is on. In order to get an accurate estimate of $\text{P}_{\text{WP}}/\text{P}_{\text{GM}}$ I monitored the total energy use of the GeoMax2 and the water pump over a 10.5 day period when no one was in the house and hence the pump came on only when water was demanded by the GeoMax2. During this 10.5 day period the average daily energy consumption of the GeoMax2 and water pump was 10.02 kWh and 3.85 kWh per day, respectively. Assuming $\text{P}_{\text{WP}}/\text{P}_{\text{GM}} = 3.85/10.02$, I have estimated

average $P_{WP} = 1.06$ kW. Hence the combined power of the GeoMax2 + water pump = 3.81 kW = 12,990 BTU/h. Hence we can calculate:

$$\text{EFFICIENCY of GeoMax2} = 100\% \times (45,160/12,990) = 348\%$$

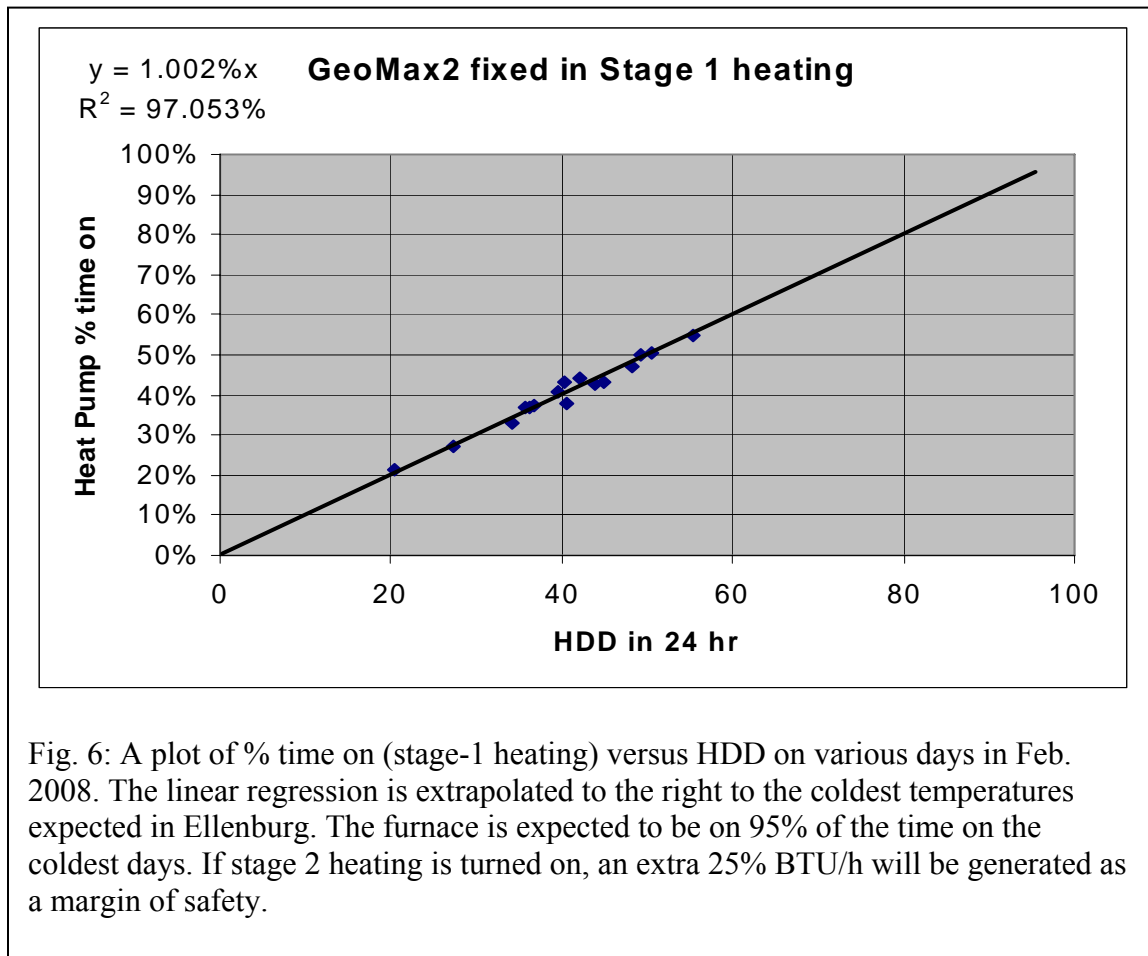
The probably error in power measurements is $\cong 0.2\%$, uncertainty of the air temperature measurement is 0.2 to 0.3 °F out of 28 °F $\cong \pm 1\%$ but the uncertainty on the control of air flow is about 5% (of CFM), hence the overall uncertainty in E is probably about 348% $\pm 18\%$ (= 5.1% x 348%).

Estimated Annual Heating Cost in my Home

The number of BTUs needed to heat any given home depends on the heat loss from the insulated envelope of the house and the HDD = heating degree days. I monitored the energy consumption of the GeoMax2 and the water pump over 40 days when the total number of HDD was 2,216. The energy consumption per HDD was 0.93 kWh/HDD. The average winter in Ellenburgh, NY, has 8010 HDD, hence during the average winter my home can be heated at an energy cost of 7,449 kWh. At the current price of electrical energy (17.1 cents per kWh) the annual heating cost is \$1,274 per year.

Is My GeoMax2 Sized Appropriately for My Home and Climate?

Of course I did the appropriate calculations initially. I computed R-values of wall, roof, windows, basement etc and did the projections for the coldest probable days. However, you never know if your builder can deliver on the promised R-values. So the ultimate test is to see what percentage of the time the GeoMax2 is on in real-world situations. Hence for the month of February 2008, I measured the % of the time on versus HDD. The data in Fig. 6 are quite linear and have been extrapolated to the right to the coldest it is likely to be in Ellenburg, NY.



Conclusions: The overall efficiency of a GHP will change from site to site. The factors determining this are the temperature of the heat exchange fluid (48 °F in my open loop well application). But in closed loop systems the fluid temperature is often lower (28 to 42 °F) causing a reduction in COP. COP is also influenced by pumping rate; COP increases with pumping rate. However there is a tradeoff in overall efficiency because high pumping rates require more energy to pump water. The pump in my application was an energy efficient Grundfos SEQ series pump operating at household water pressure (50 psi). The efficiency of the GHP would be improved by reducing the pump pressure for the GHP to, say, 20 psi and adding a booster pump to for the domestic water supply. More testing would be required to determine if this might a cost-effective solution in terms of dollars saved in annual heating costs versus cost of the extra hardware. The factory claims an overall COP of 4.4 for the GeoMax2 in stage-1 heating. The figure I got was 4.82 ± 0.24 . The factory value was based on different test conditions: slightly warmer water (50 °F vs 48 °F at my site) but lower water flow rate (probably 7.5 GPM vs 9.5). It is not clear if my COP is significantly higher from the factory value because no statistics are available from the factory.